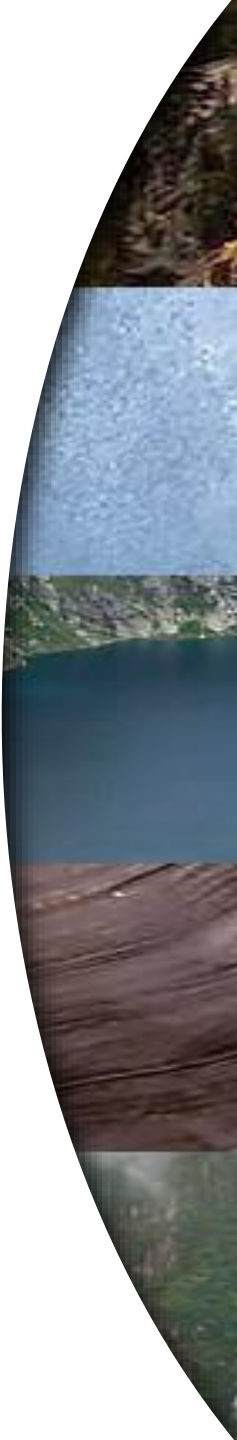


# Safe Cracking: Monte Carlo Nonlinear Coupled Analysis of Nuclear Reactor Bricks

Quintessa support to EDF Energy

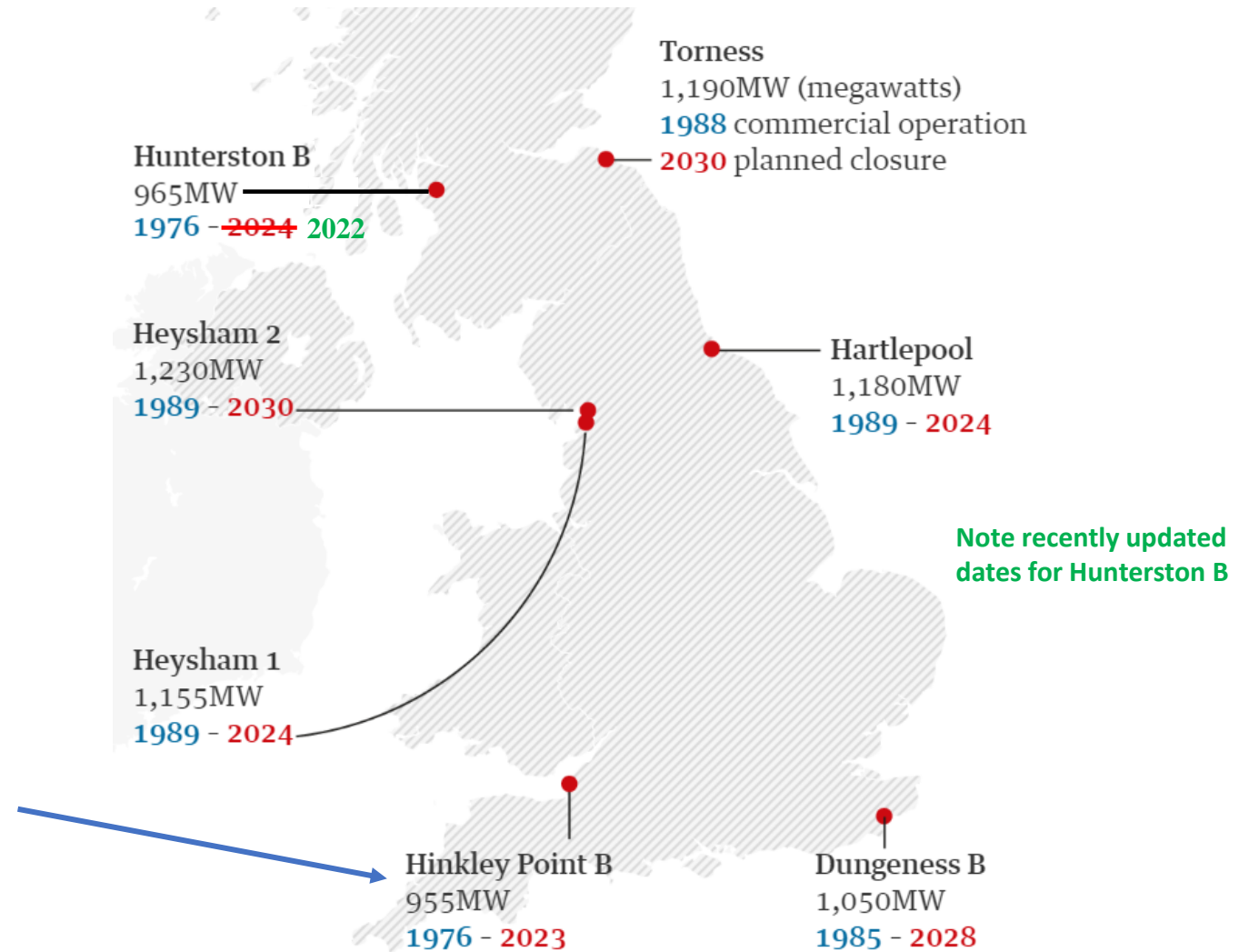
Alex Bond, Mark Pogson, Peter Robinson

November 2020



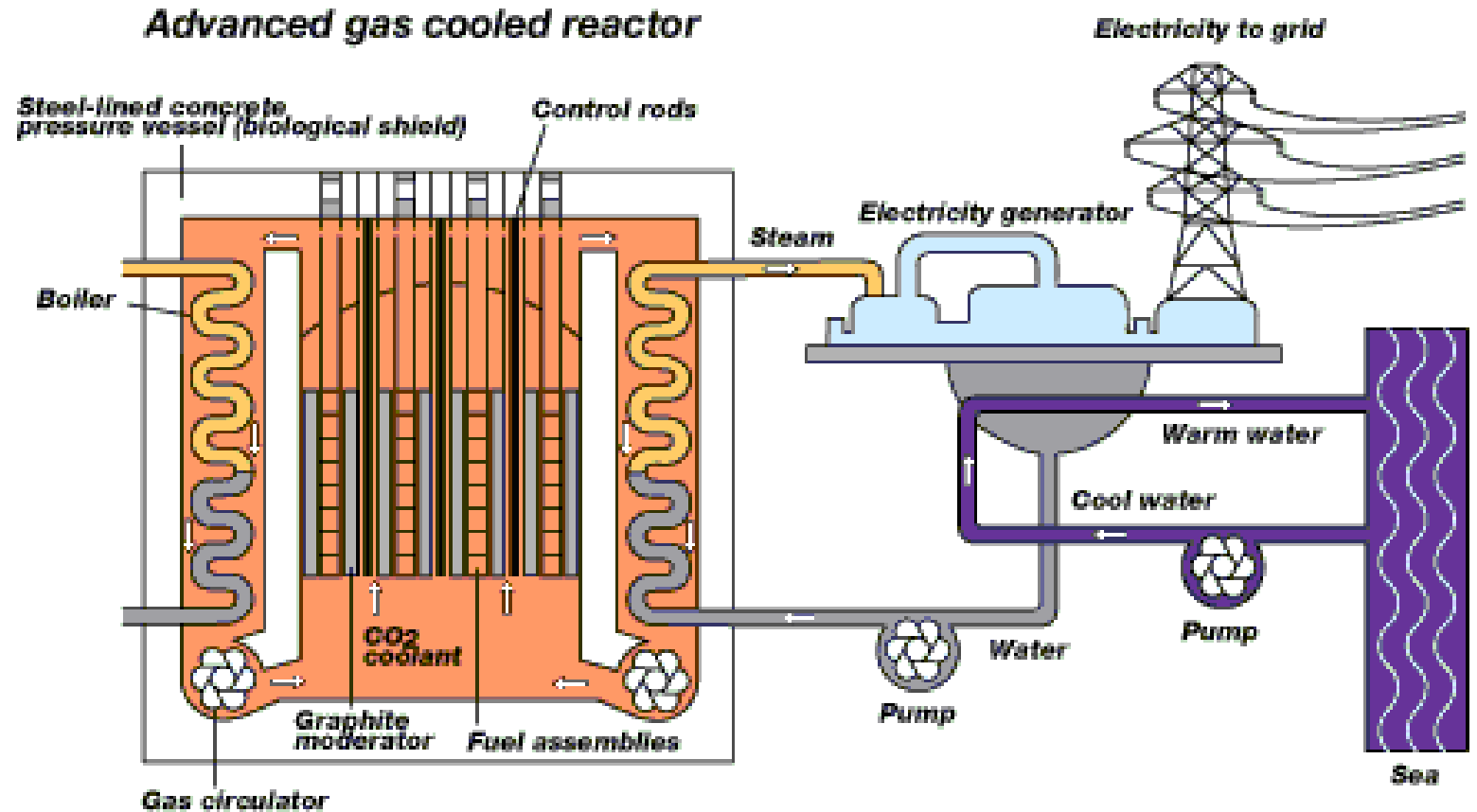
# Advanced Gas-cooled Reactors (AGRs)

- AGRs provide around 15% of UK power
  - Owned and operated by EDF Energy
- All are expected to reach end of life over the next decade or so
  - New builds not generating until ~2025
- Quintessa provides modelling support to help understand and predict the behaviour of bricks in the reactors



# AGR Design

- Nuclear fuel rods are suspended in channels of graphite bricks, which provide moderation
- Gas-cooled (40 bar CO<sub>2</sub> at ~450 °C)
- Graphite bricks are expected to be the limiting factor in the lifespan of most AGRs



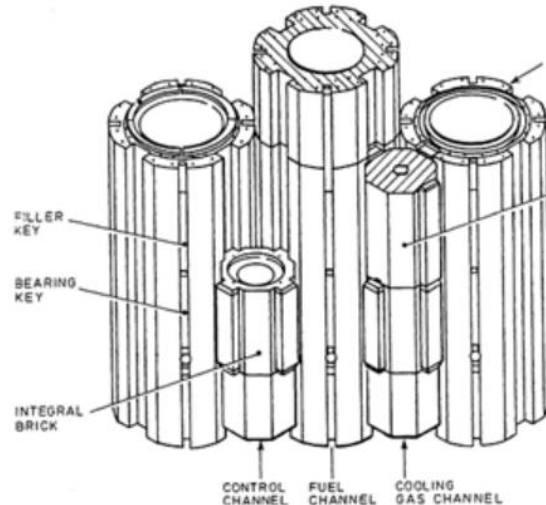
# What is the issue?

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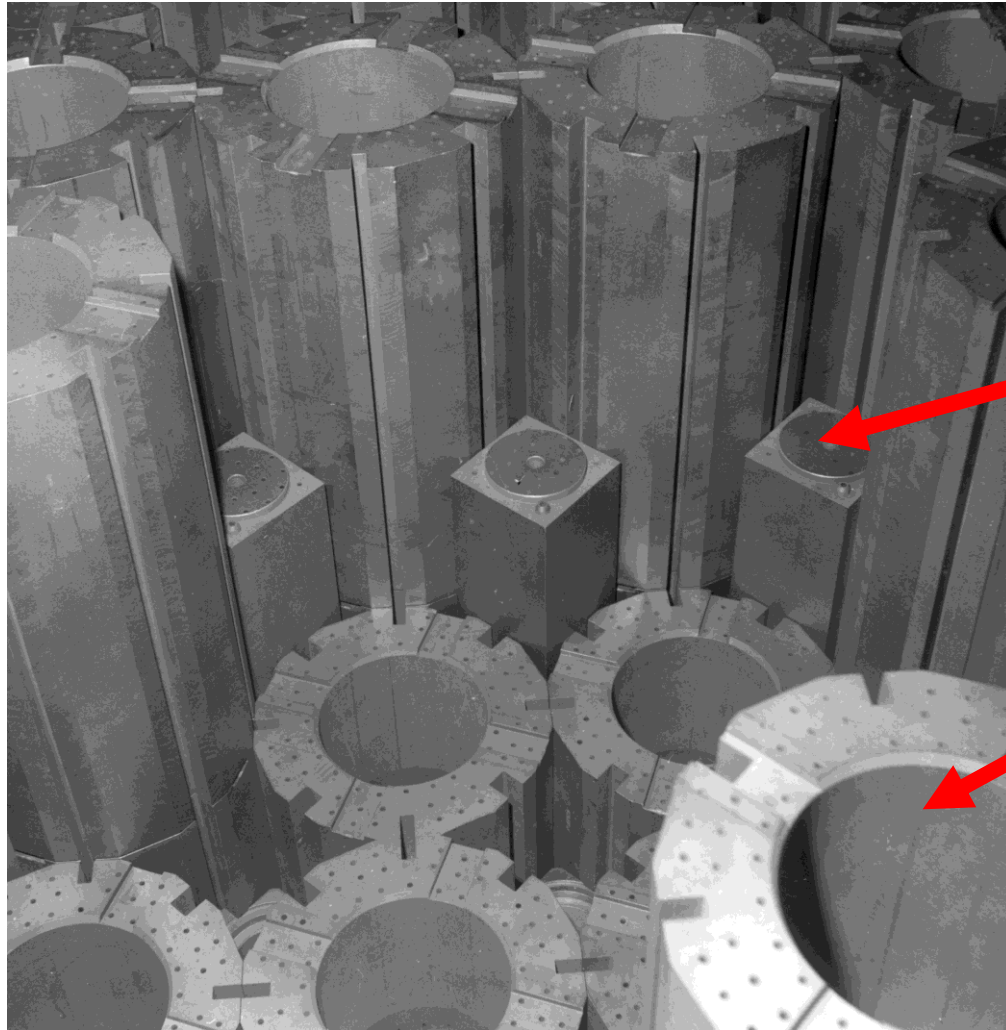
- Reactors are expected to operate until 2022-2030 (depending on the individual reactor)
- Some already had a lifetime extension for safe operation
- New nuclear build (e.g. Hinkley C) not expected to start providing electricity until ~2025
- Keeping these reactors running is important to maintain UK energy mix (nuclear provides valuable 'base-load')
- Reactors continue to age. Main area of challenge is on the distortion and geometry of the graphite core
- Continued safe operation is kept under constant review and scrutiny by ONR. EDF Energy delivers regular safety cases to demonstrate sufficient understanding of the core state to permit continued safe operation

# Graphite Bricks

- Graphite makes up the bulk of the core
- Conditions for the bricks are incredibly hostile
  - High temperatures ( $\sim 400+^{\circ}\text{C}$ ) – **thermal expansion**
  - High flux of neutrons – causes graphite atoms to be knocked out of place – **changes to material properties**
  - High pressure and temperature  $\text{CO}_2$  – chemical changes resulting in **loss of graphite** as the reactor ages



# Graphite Core Detail



Details vary between stations  
Hinkley/Hunterston (left)  
Hartlepool/Heysham (right)

Interstitial Brick

Fuel Brick

Brick Height: ~830-900mm  
Brick Radius: ~230mm

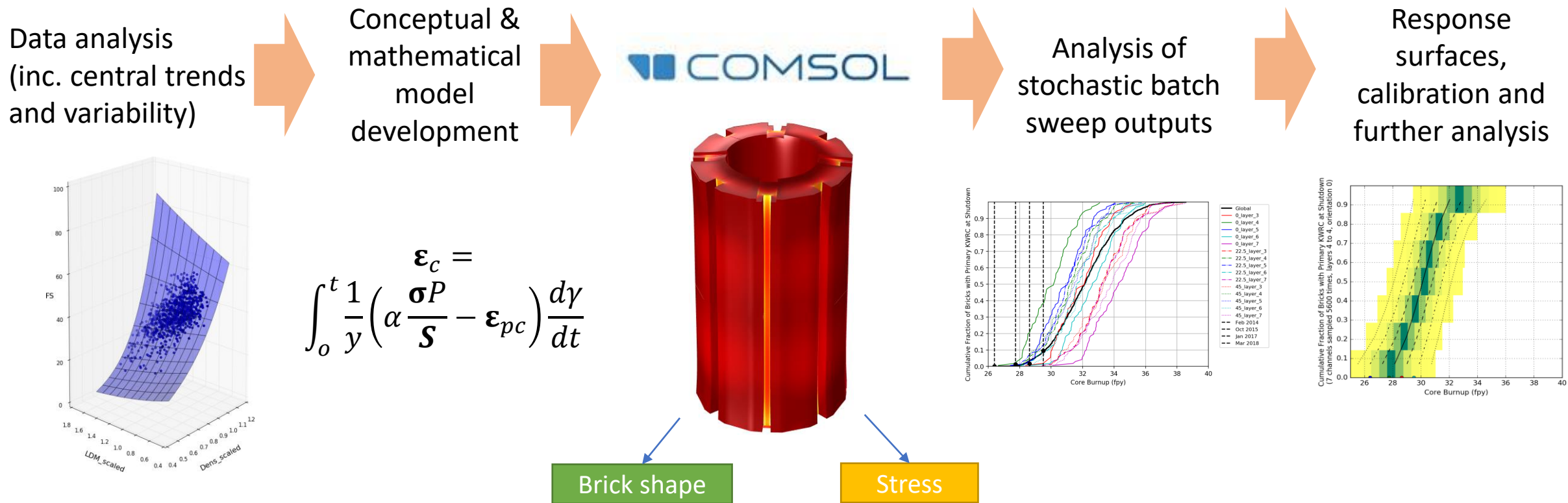
Radial keyway

End face  
keyway

Keyway root and  
illustrative crack to  
brick bore

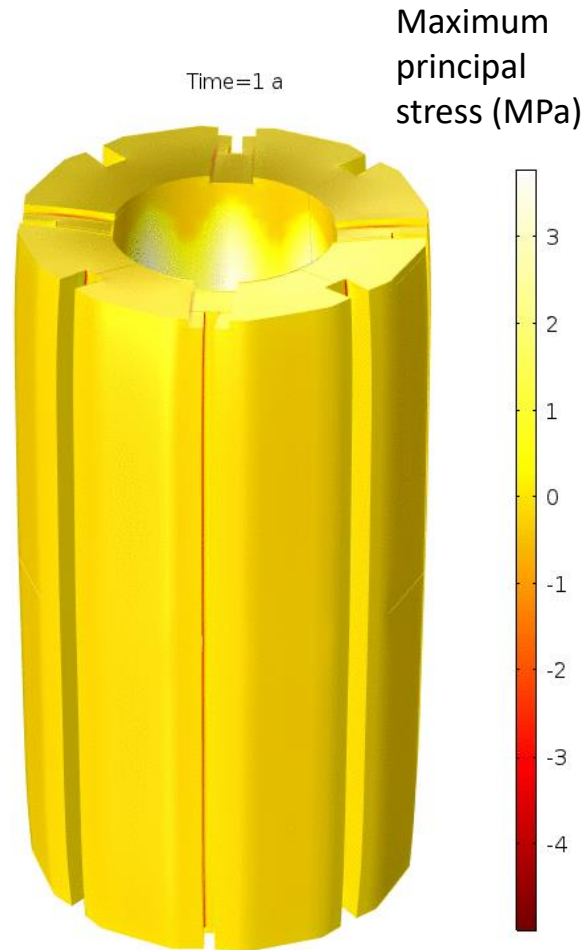
# Modelling Overview

COMSOL is at the centre of a 'diverse' modelling route used by Quintessa to predict brick cracking rates, accounting for variability between bricks



$$\epsilon_c = \int_0^t \frac{1}{y} \left( \alpha \frac{\sigma P}{S} - \epsilon_{pc} \right) \frac{dy}{dt}$$

# COMSOL Simulation

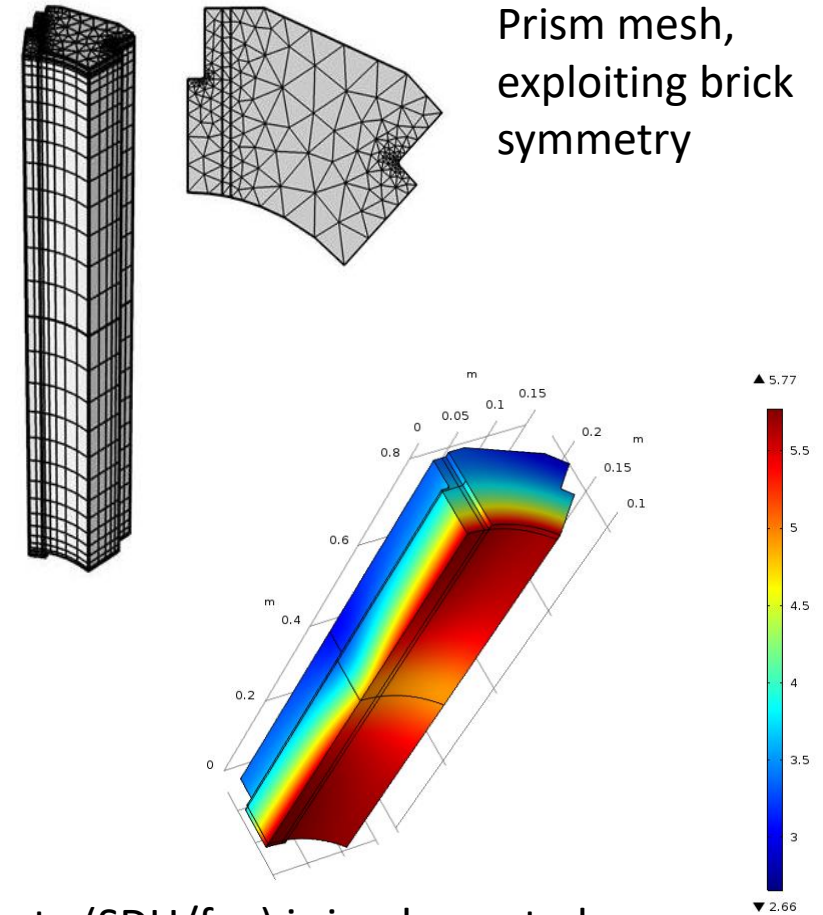


- Each brick is simulated over 40 full power years (fpy)
- Brick shape evolves due to 'dimensional change' process driven by neutron dose (shape goes from barrel → wheatsheaf)
- In later life, stresses concentrate in keyways, which can lead to keyway root cracking (KWRC)



# COMSOL Implementation

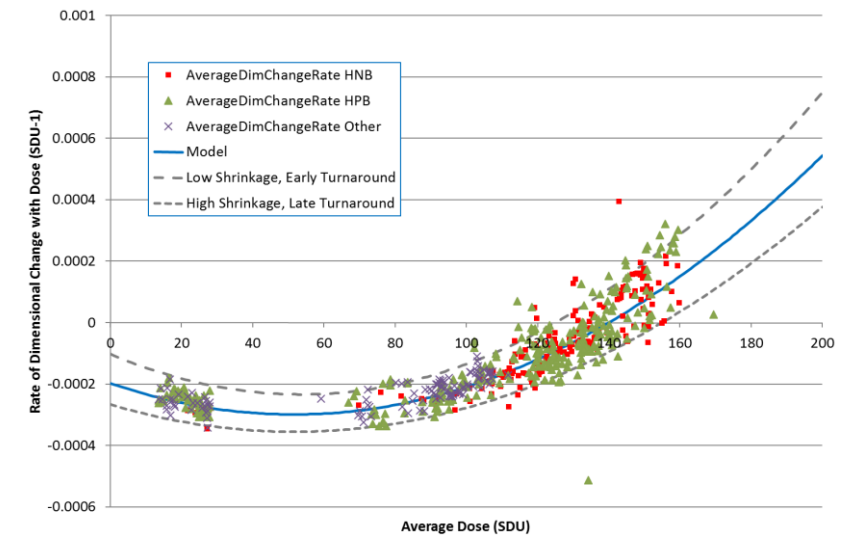
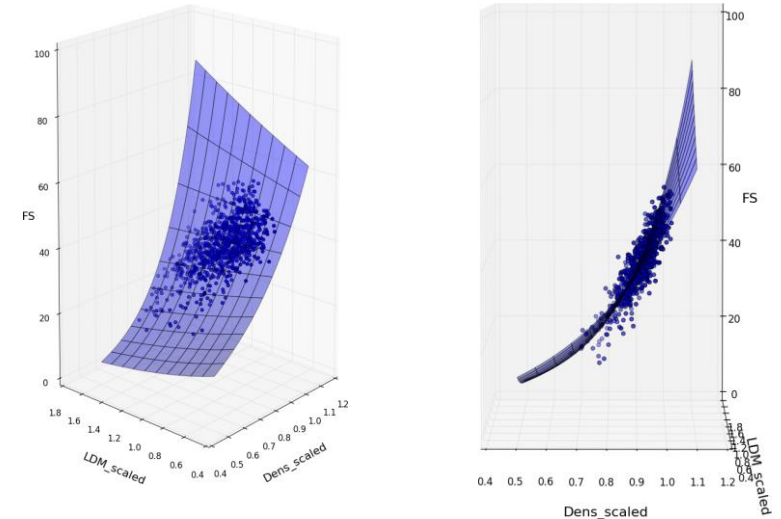
- Custom physics coupled with **Structural Mechanics** module using ODE interfaces
- **Batch Sweep** Monte Carlo simulation accounts for brick variability in physical properties
  - Dimensional Change (DC), Creep, Dose, Weight Loss, Dynamic Young's Modulus, Flexural Strength (FS), Coefficient of Thermal Expansion
- 256 bricks simulated per layer using independently sampled parameters, 'at power' and 'at shutdown'
- Run time of ~1 hr per case



Dose rate (SDU/fpy) is implemented as a field variable, similarly to temperature

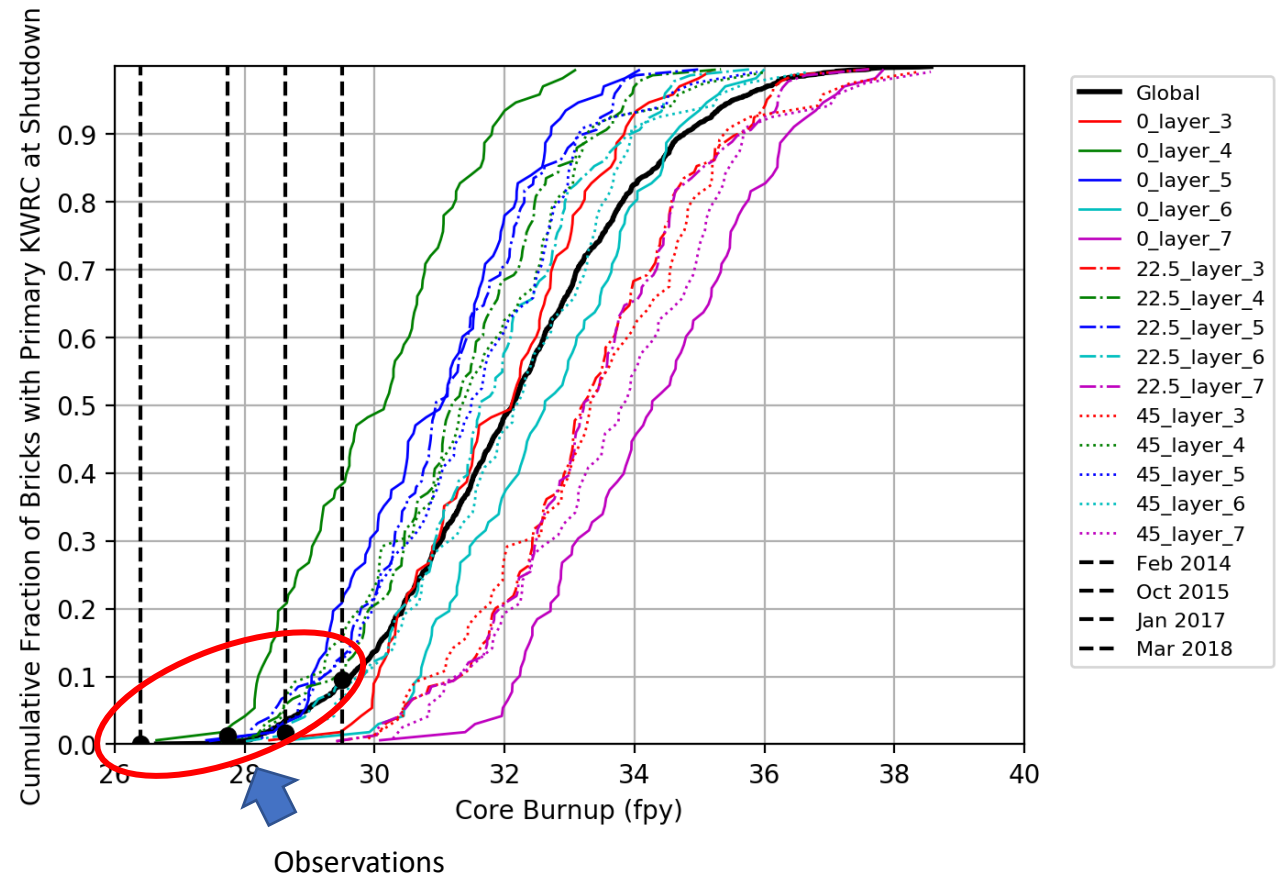
# Underlying Statistical Modelling

- AGR-specific data collected every ~12 months (at reactor shutdowns)
  - Trepan data (small-scale boring of graphite bricks)
  - Bore shape data (diameter measurements)
  - Camera inspection data (identifies keyway root cracks)
- Also have material test reactor MTR data for dimensional change
  - Small samples not in true AGR conditions, so considerable uncertainty
- These data are used to construct statistical models of graphite properties
  - Model forms are constrained to be physically plausible
  - Allows brick-to-brick variability to be characterised quantitatively
  - Easier to implement and validate than mechanistic models



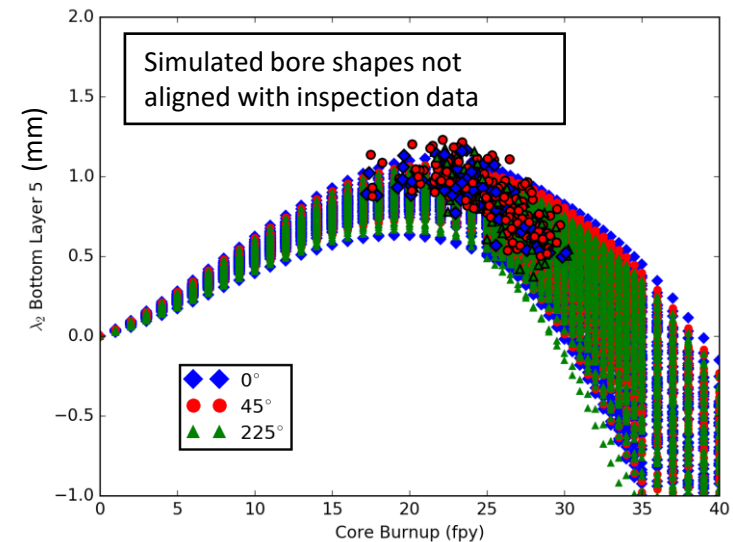
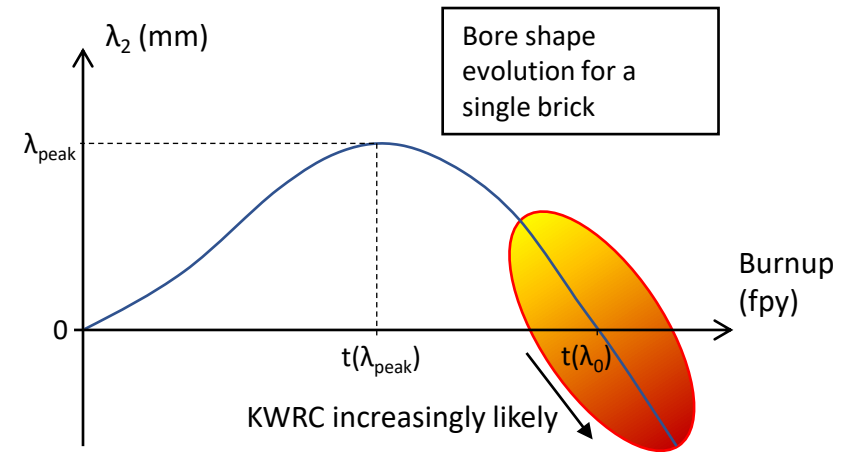
# Uncalibrated KWRC Rates

- KWRC times are calculated from the ratio of maximum in-plane principal (MIPP) stress relative to FS
  - Threshold of 1.5 from lab tests but with considerable uncertainty
- All cracks are predicted to occur when the reactor has been cooled for inspection (noting that any cracking caused by brick interaction is not modelled here)
- Predictions in good agreement with observations
  - No global calibration has been performed here – only fitting of each property to AGR data (MTR for DC)



# Bore Shapes

- Bore shape is characterised by  $\lambda_2$  measurement
  - Bore radius difference:  $\lambda_2 = r_{\text{mid}} - r_{\text{end}}$
- Bricks bulge out early in life before contracting later (barrel  $\rightarrow$  wheatsheaf)
  - KWRC more likely as  $\lambda_2$  decreases
- There is an offset apparent between predictions and observations
  - Suggests DC parameter distributions are not quite right (noting use of MTR not AGR data)
- Therefore need to calibrate the model as a whole, not just to individual properties
  - But COMSOL model slow to run

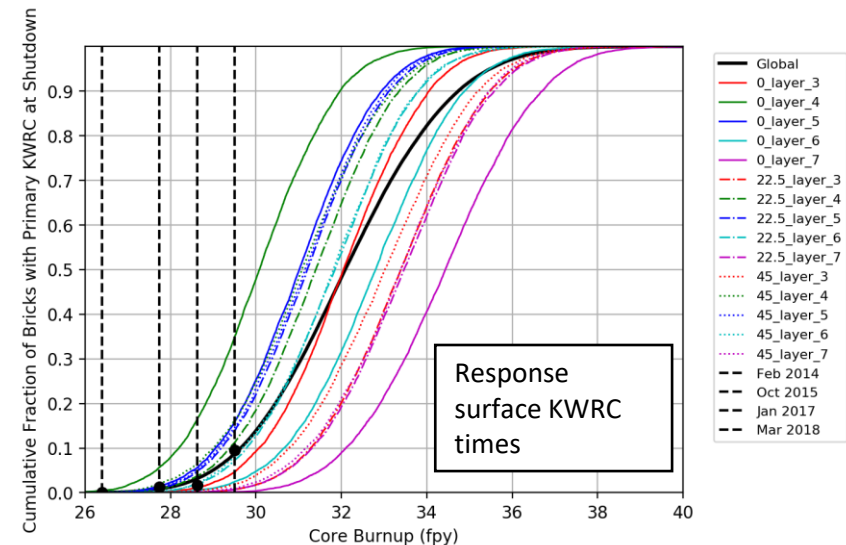
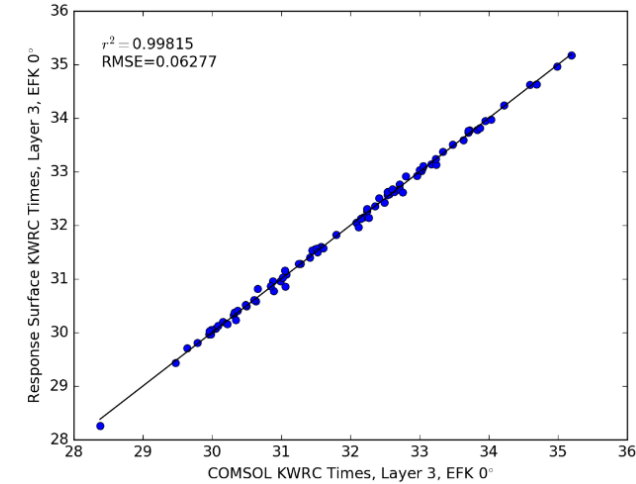


# Response Surface (Surrogate model)

- Low-order polynomial is used to approximate COMSOL results, with parameters grouped by property

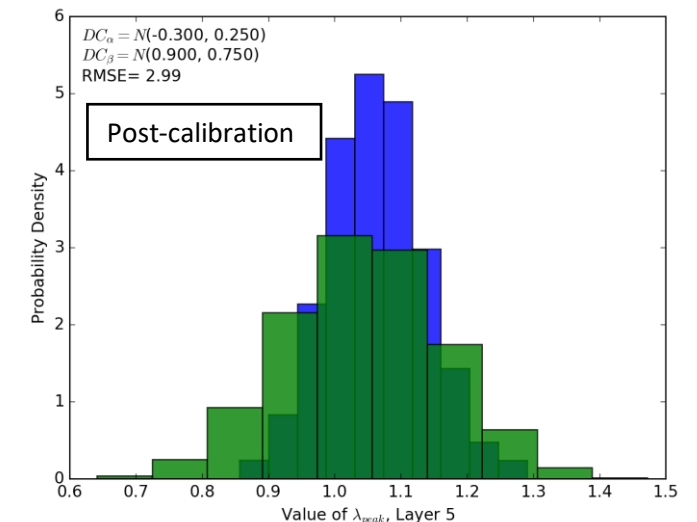
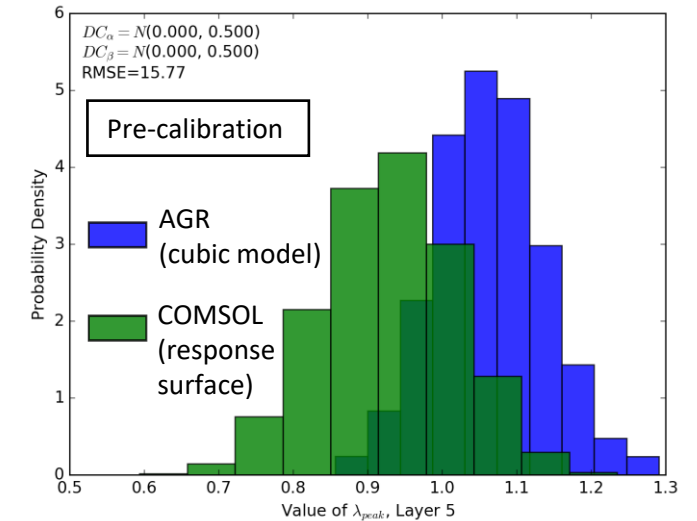
$$\begin{aligned}
 R = & (c_0 + c_{FS}S_{FS} + c_{DYM}S_{DYM} + c_{WL}S_{WL} + c_{\alpha X}\alpha_{DC}) \\
 & \times (1 + c_{\alpha}\alpha_{DC} + c_{\beta}\beta_{DC} + c_{\alpha\beta}\alpha_{DC}\beta_{DC}) \\
 & \times (1 + c_C F_C) \times (1 + c_{CTE}S_{CTE}) \\
 & \times (1 + c_{D_{self}}S_{D_{self}} + c_{D_{side}}S_{D_{side}} + c_{D_{corner}}S_{D_{corner}})
 \end{aligned}$$

- Coefficients  $c$  are fitted to variable  $R$  from COMSOL outputs
  - Originally developed to model time of KWRC
  - Also predicts other variables well, e.g.  $\lambda_2$ ,  $t(\lambda_2)$
- Far greater sample sizes can be used than with COMSOL

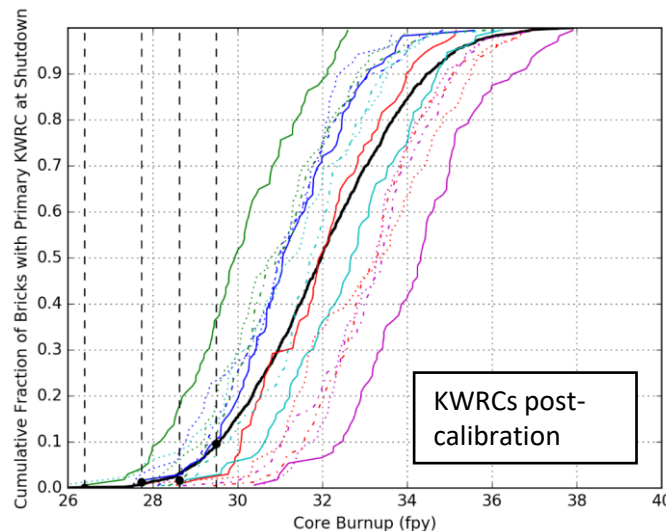
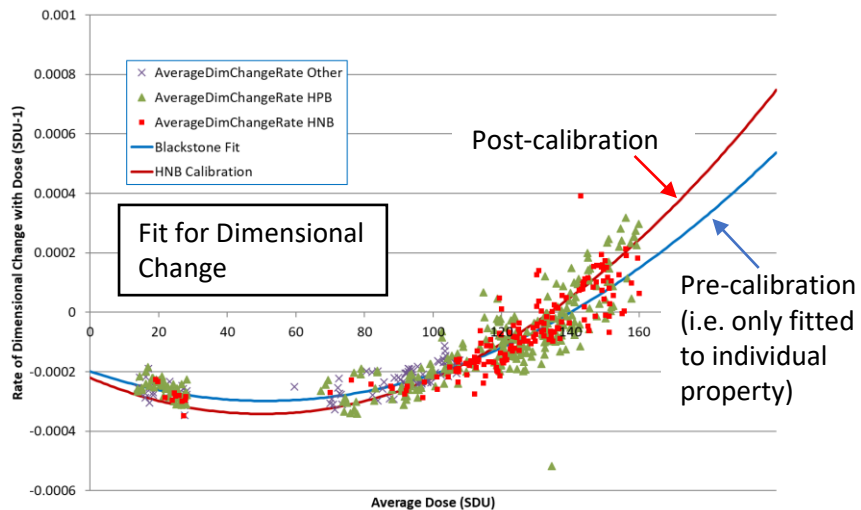
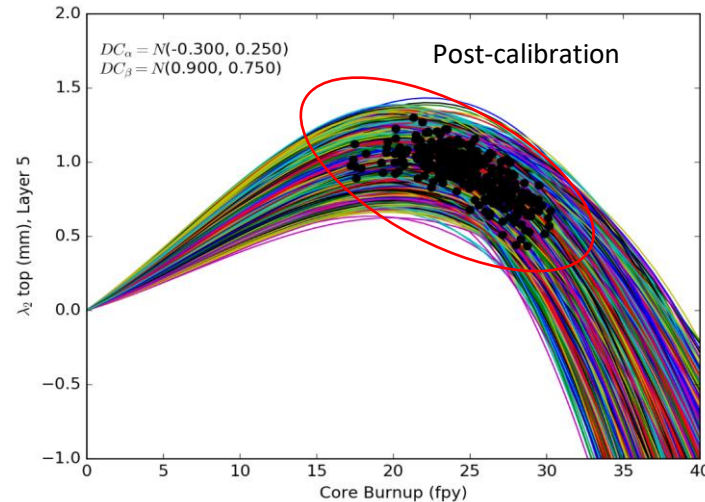
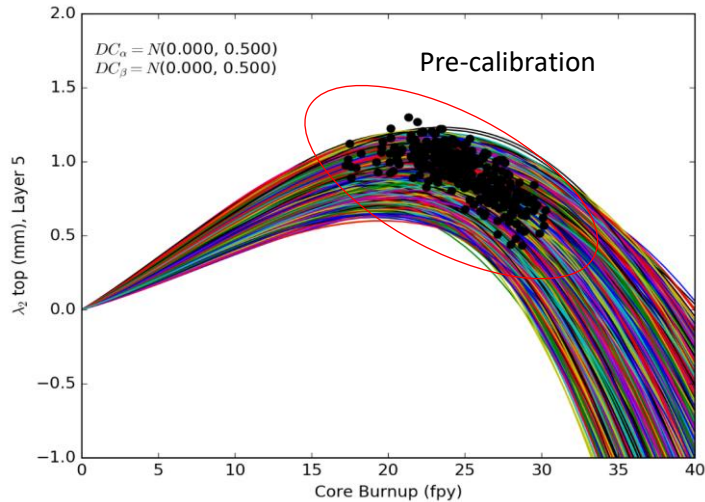


# Calibrating to Bore Shape

- The response surface is fitted to bore shape features of  $\lambda_{\text{peak}}$ ,  $t(\lambda_{\text{peak}})$  and  $t(\lambda_0)$ 
  - These features are then predicted using multiple brick samples
- The same bore shape features are estimated using a cubic model fitted to inspection data for individual bricks
- Distributions of the features are compared between the cubic model and response surface
  - By varying DC parameter distributions used in the response surface, differences in features are minimised by optimisation
- Calibrated parameter distributions are required to be consistent across layers and features



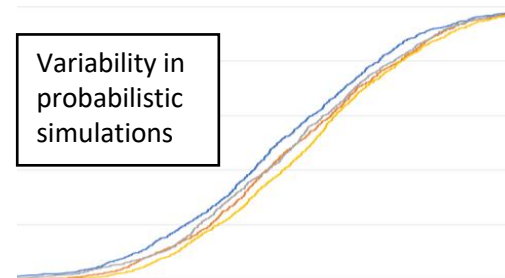
# Calibration Result



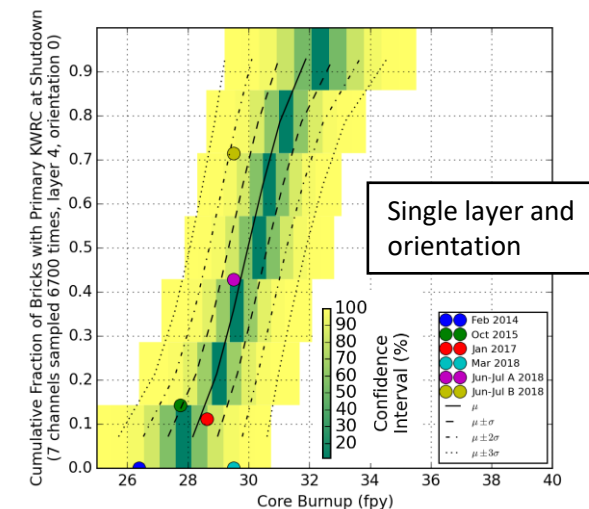
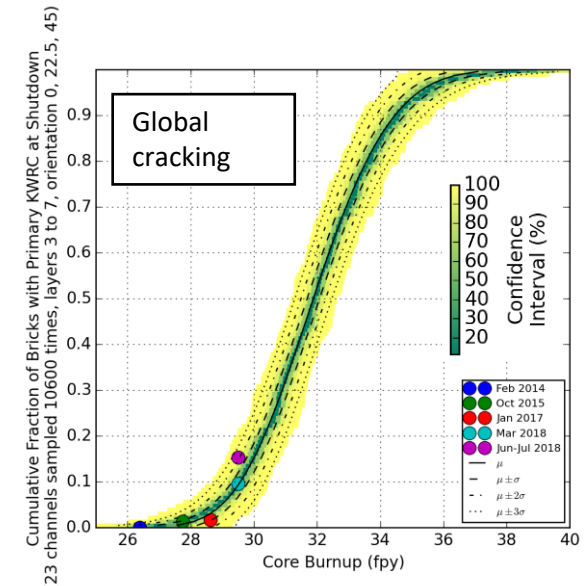
- The new parameter distributions improve agreement with bore shape evolution data
  - Fits for individual physical properties also remain good
- Small adjustment to failure model on keyway root to recalibrate
  - This is well within its uncertainty, and also accounts for differences in modelled temperatures
- Transparent calibration process
  - Builds confidence in model
  - Allows further analysis using response surface

# Comparison with Observed KWRCs

- The response surface can also be used to estimate KWRC uncertainties
  - Each Monte Carlo simulation gives slightly different results, so repetition captures inherent variability
  - The calibrated DC parameters (using AGR data) help to support predictions of variability



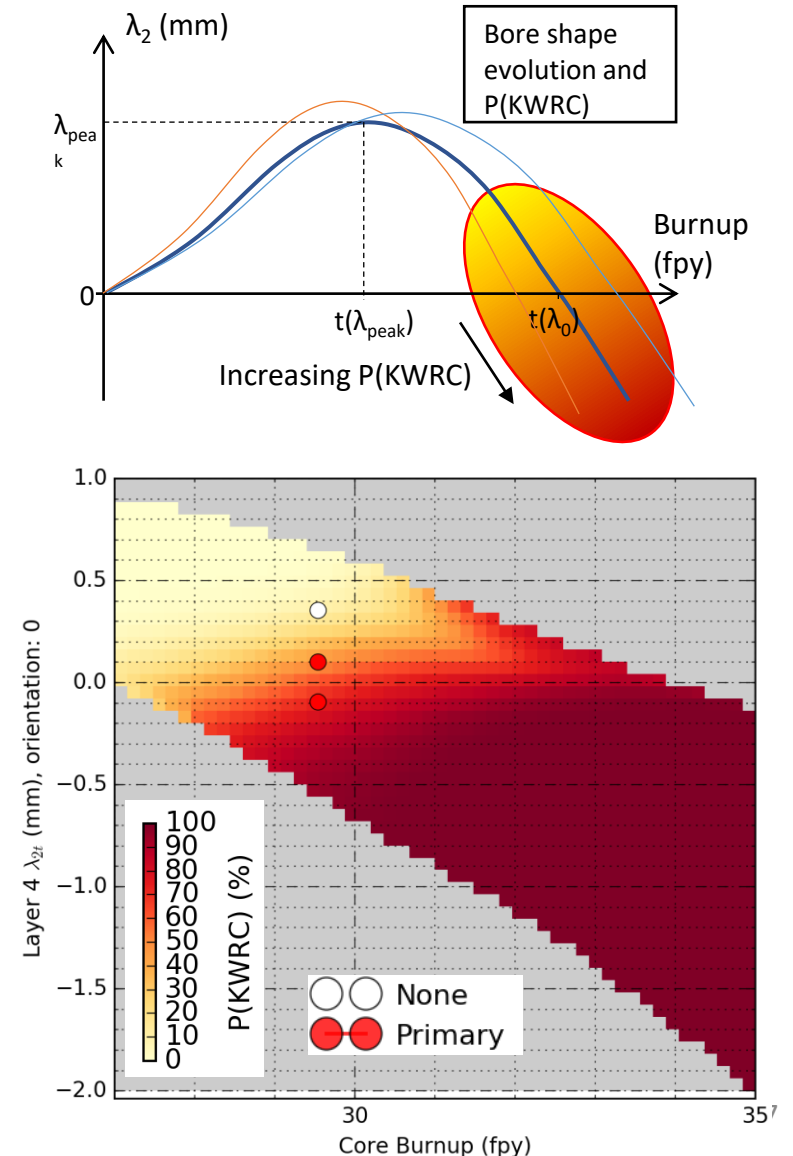
- The sample size can be fixed to match the number of inspection channels
  - Confidence intervals are estimated by repeated simulation using the fixed sample size
  - Large uncertainties exist with limited channels and layers – important to note for comparison with observations





# Understanding Data, Building Confidence

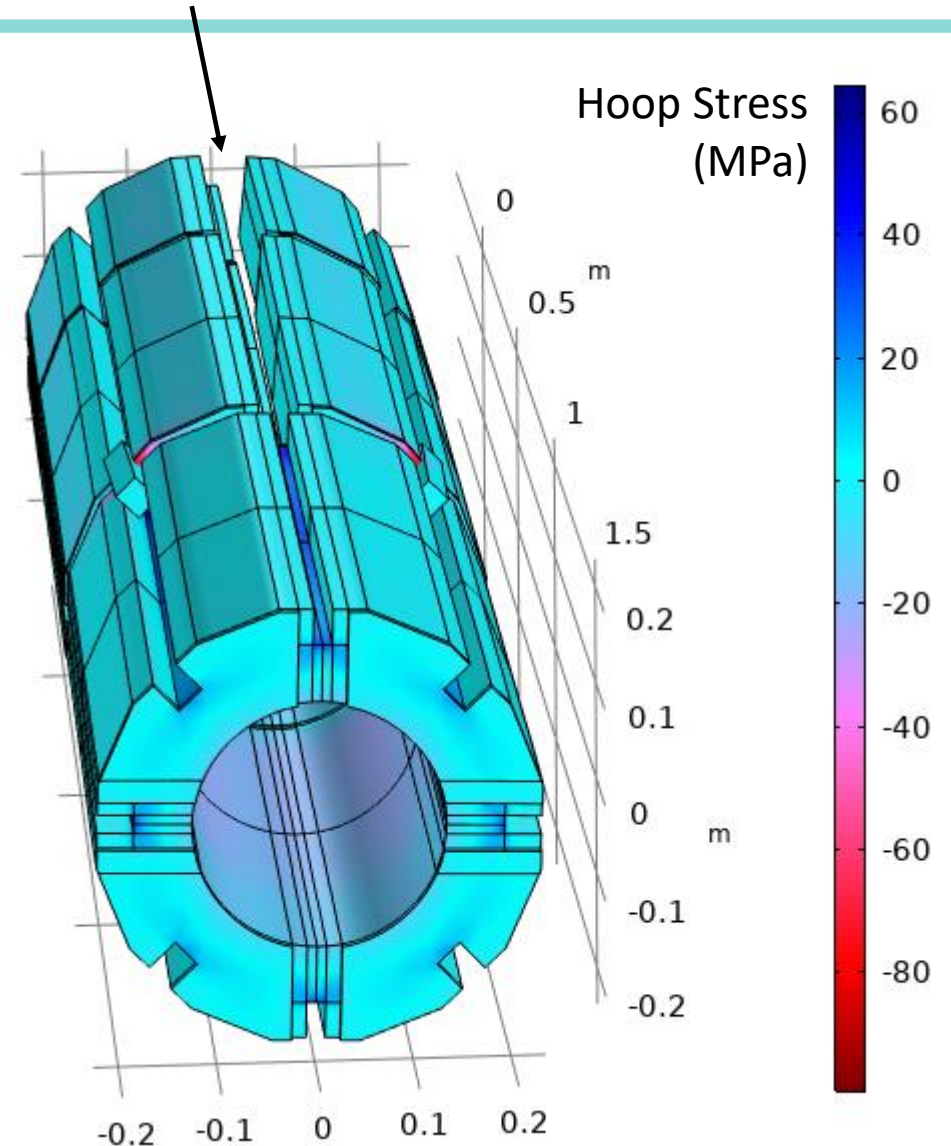
- Multiple types of cracks expected to be seen in reactor, not just 'primary' keyway root cracks.
- Method can be used to say how likely we expect a crack is to be a primary keyway root crack given the reactor age and bore shape
- Can also be used to build confidence in the modelling method



# Multiple Bricks

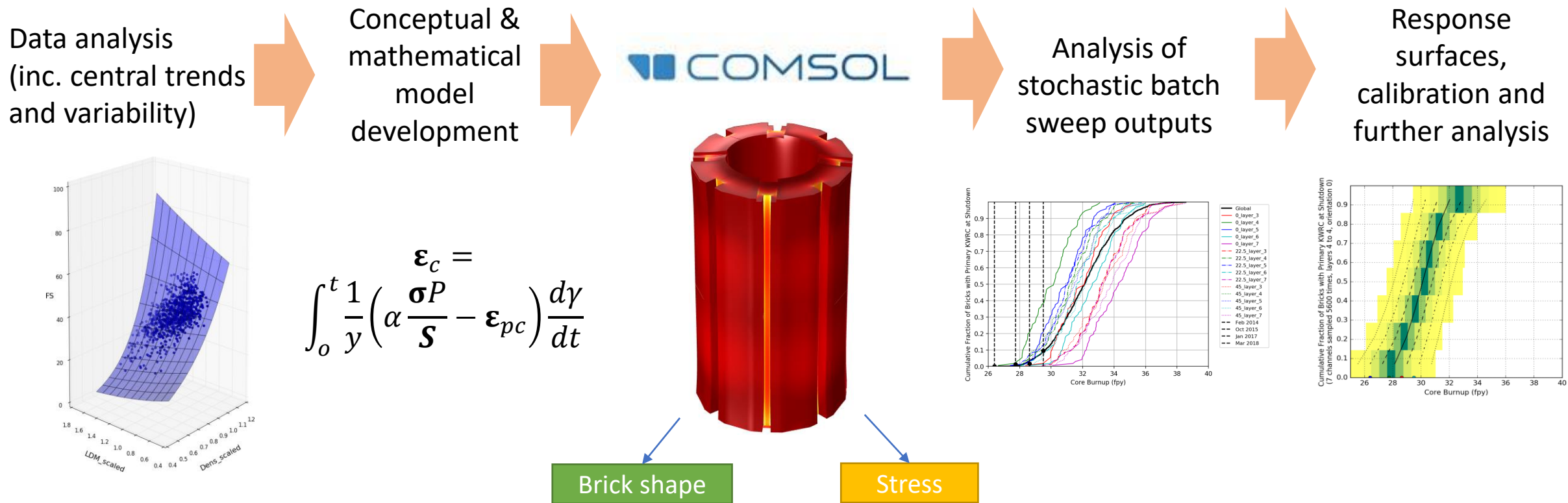
- Currently investigating multiple bricks interacting
- Having cracked, can get significant interaction via the keying system, accelerating cracking in adjacent bricks
- Initial work matches with observations

Simulated keyway root cracks



# Modelling Overview (revisited)

COMSOL is at the centre of a 'diverse' modelling route used by Quintessa to predict brick cracking rates, accounting for variability between bricks



# Summary

- Understanding the state of the graphite core of AGRs is a key component in their continued safe operation
- COMSOL is being used as an 'engine' in a statistical and stochastic modelling approach by Quintessa to help understand the core state
- Sincere thanks to all in the EDF Energy Graphite Branch, especially Mark Bradford, Sam Baylis and Jim Reed

